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Engineering Geodesy

Automatic Lateral Control of a Model Dozer

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Structure

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Motivation

- machine control and guidance is one of the current research topics in engineering geodesy
- accuracy requirements: 50 mm in position
up to 5 mm in height

at IIGS a hardware-in-the-loop simulator has been built up

Position measurements by tachymeter (highest accuracy)

up to now, only wheeled vehicles are integrated

Machine	height accuracy	position accuracy	velocity	available systems
Dozer/Scraper	20 - 30 mm	20 - 50 mm	up to 3 m/s	I+II
Digger	20 - 30 mm	20 - 30 mm		
Asphalte Paver	5 mm	5 mm	up to 0,16 m/s	I+II+III
Concrete Paver	5 mm	5 mm	up to 0,05 m/s	I+II+III
Curb & Gutter Pav.	5 mm	5 mm	up to 0,08 m/s	I+II+III
Milling machine	15 - 10 mm	10 - 20 mm	up to 0,30 m/s	I+II
Roller	-	10 - 20 mm	up to 3 m/s	I+II

New possibilities by integrating a dozer!

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Steering of tracked vehicles

Concentration on two track crawlers: the dozer model

	Circle Drive	Rotation	Crab Steering Mode	Small Circle Drive
Two-Track Crawler Chassis				
Three-Track Crawler Chassis (symmetric)				
Three-Track Crawler Chassis (not symmetric)				see Circle Drive
Four-Track Crawler Chassis				

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The dozer model

track velocities
 $v_r = r \cdot \omega_r$ and $v_l = r \cdot \omega_l$
r – roller radius / ω - angular velocity

dozer velocity

$$v = \frac{v_l + v_r}{2}$$

radius

$$R = \frac{B \cdot v}{v_r - v_l} = \frac{B \cdot (v_l + v_r)}{2 \cdot (v_r - v_l)}$$

B – distance between the two tracks

orientation change

$$\Delta\varphi = \arctan\left(\frac{(v_l - v_r) \cdot \Delta t}{B}\right)$$

without slippage

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The dozer model

slip values

$$i_l = \frac{v_l - v'_l}{v_l} \text{ and } i_r = \frac{v_r - v'_r}{v_r}$$

v – actual velocity
v' – roller velocity

track velocities

$$v_r = r \cdot \omega_r \cdot (1 - i_r) \text{ and } v_l = r \cdot \omega_l (1 - i_l)$$

Further computations
 as in case without slippage.


with slippage

Not considered for dozer model implementation !


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Integration of dozer model into simulator

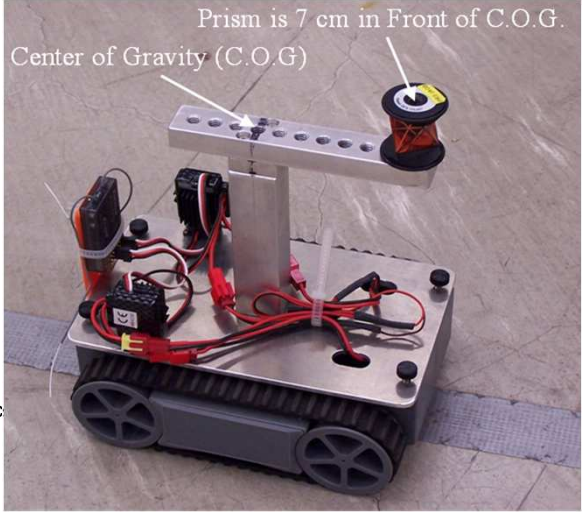
Tachymeters:
Leica TS30 and TCRP 1201,
Trimble SPS930

Reflector: Leica GRZ 101

Computer and remote control


Dozer model 1:14

Trajectory length: 11 m
2 straight lines, 4 clothoids, 2 arc
Point distance: 0.1 m




Prism is 7 cm in Front of C.O.G.
Center of Gravity (C.O.G)

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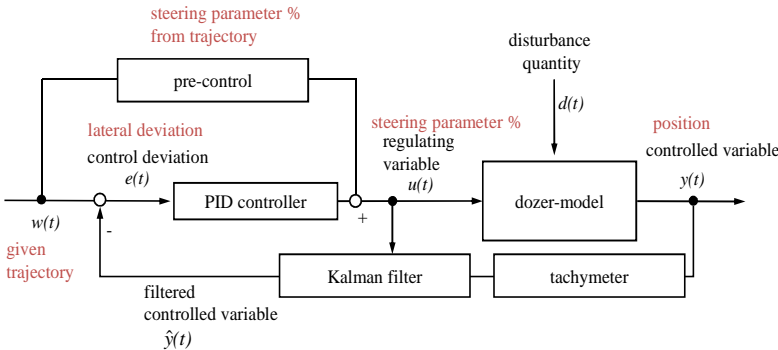


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Integration of dozer model into simulator: Closed control loop




The diagram shows a closed-loop control system. The input is a 'given trajectory' $w(t)$. This signal is compared with the 'filtered controlled variable' $\hat{y}(t)$ to produce a 'lateral deviation control deviation' $e(t)$. This error signal is processed by a 'PID controller' to generate a 'steering parameter % regulating variable' $u(t)$. This signal is added to a 'pre-control' signal and then sent to the 'dozer-model'. The 'dozer-model' also receives a 'disturbance quantity' $d(t)$ and produces a 'position controlled variable' $y(t)$. This output is measured by a 'tachymeter' and processed by a 'Kalman filter' to produce the 'filtered controlled variable' $\hat{y}(t)$, which is fed back to the input summing junction.


steering parameter:

$$p = \frac{v_r}{v_l} \cdot 100$$

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Steering calibration

Velocity in dependence of p :


$$v = \frac{v_l + v_r}{2} = \frac{v_l \cdot (1 + \frac{p}{100})}{2} \quad v_l = \frac{2 \cdot v}{1 + \frac{p}{100}} \quad \text{and} \quad v_r = v_l \cdot \frac{p}{100}$$

Radius in dependence of p :


$$R = \frac{B \cdot v}{v_r - v_l} = \frac{B \cdot (1 + \frac{p}{100})}{2 \cdot (\frac{p}{100} - 1)}$$

- Calibration is relationship between p and curvature $1/R$.
- p is a ratio of two velocities.
- Velocities are proportional to voltages for given velocities.
- The velocities driven are 6 cm/s and 10 cm/s.

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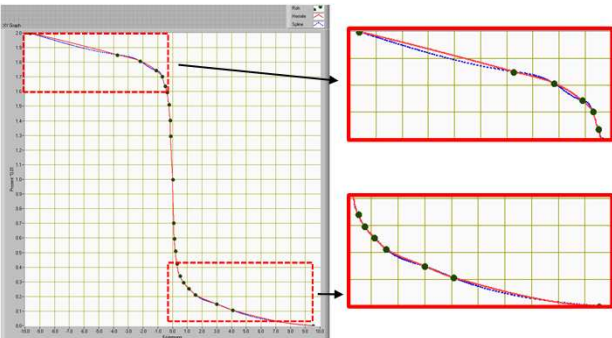


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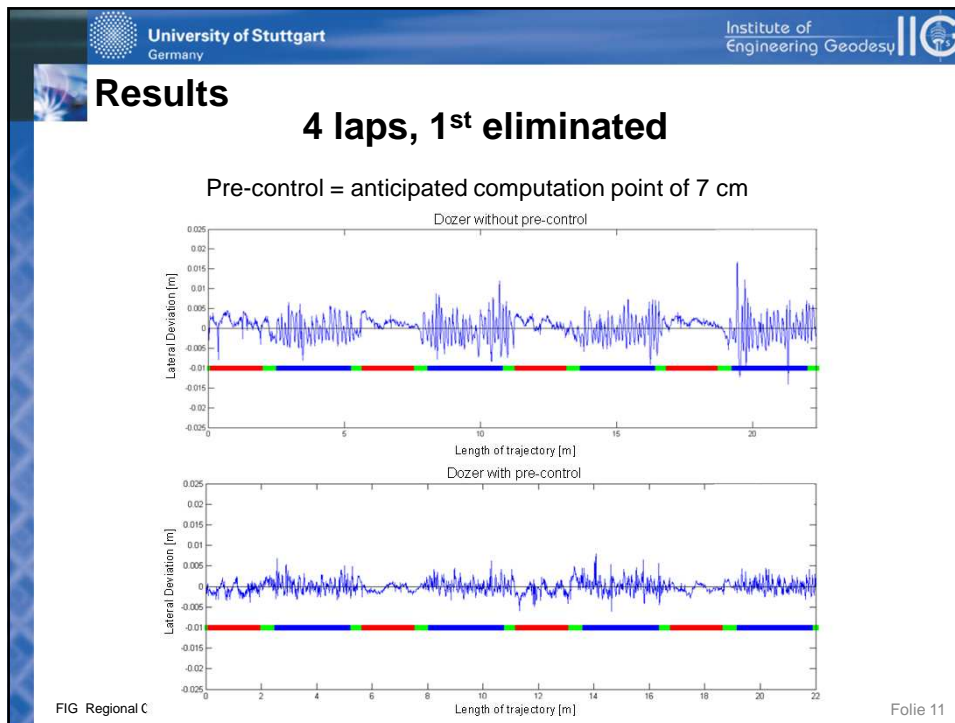
Steering calibration

Non-linear calibration function



Hermite interpolation (red) and spline interpolation (blue)

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Results

Dozer without pre-control [m]				
	straight	clothoid	circle	total
Lap 2	0.002	0.003	0.003	0.003
Lap 3	0.002	0.003	0.004	0.003
All Laps	0.002	0.003	0.004	0.003

Dozer with pre-control [m]				
	straight	clothoid	circle	total
Lap 2	0.001	0.001	0.002	0.002
Lap 3	0.001	0.003	0.002	0.002
Lap 4	0.001	0.002	0.002	0.002
All Laps	0.001	0.002	0.002	0.002

Pre-control improves solution by 1 mm / 50 % !

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Results

Kalman filter doesn't improve the RMS, but trajectories are smoother !

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Conclusion

Comparison to wheeled vehicles

	straight	clothoid	circle	total
Front Wheel Steering (Beetz & Schwieger 2010)				
PID-controller with pre-control	0.001	0.002	0.002	0.002
Dozer (Beetz 2012)				
PID- controller with pre-control	0.001	0.002	0.002	0.002
Rear Wheel Steering (Beetz 2012)				
Multi-value controller with disturbance transfer function	0.002	0.003	0.004	0.003

Control RMS comparable to wheeled vehicles !

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Thank you very much for your attention!

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